

### FEATURES

- Bias voltage range (VBIAS): 2.5 V to 5.5 V**
- LDO input voltage range (VIN1/VIN2, VIN3): 1.8 V to 5.5 V**
- Three 200 mA low dropout voltage regulators**
- 16-lead, 3 mm × 3 mm LFCSP**
- Initial accuracy: ±1%**
- Stable with 1 μF ceramic output capacitors**
- No noise bypass capacitor required**
- 3 independent logic controlled enables**
- Over current and thermal protection**
- Key specifications**
  - High PSRR**
    - 76 dB PSRR up to 1 kHz
    - 70 dB PSRR 10 kHz
    - 60 dB PSRR at 100 kHz
    - 40 dB PSRR at 1 MHz
  - Low output noise**
    - 24 μV rms typical output noise at V<sub>OUT</sub> = 1.2 V
    - 43 μV rms typical output noise at V<sub>OUT</sub> = 2.8 V
- Excellent transient response**
- Low dropout voltage: 110 mV @ 200 mA load**
- 85 μA typical ground current at no load, all LDOs enabled**
- 100 μs fast turn-on circuit**
- Guaranteed 200 mA output current per regulator**
- −40°C to +125°C junction temperature**

### APPLICATIONS

- Mobile phones
- Digital cameras and audio devices
- Portable and battery-powered equipment
- Portable medical devices
- Post dc-to-dc regulation

### GENERAL DESCRIPTION

The ADP320 200 mA triple output LDO combines high PSRR, low noise, low quiescent current, and low dropout voltage in a voltage regulator ideally suited for wireless applications with demanding performance and board space requirements.

The low quiescent current, low dropout voltage, and wide input voltage range of the ADP320 triple LDO extend the battery life of portable devices. The ADP320 triple LDO maintains power supply rejection greater than 60 dB for frequencies as high as 100 kHz while operating with a low headroom voltage. The ADP320 triple

### TYPICAL APPLICATION CIRCUITS

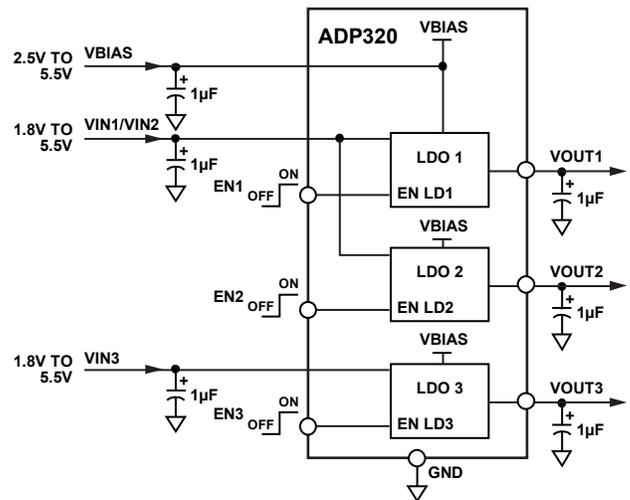


Figure 1. Typical Application Circuit

09874-001

LDO offers much lower noise performance than competing LDOs without the need for a noise bypass capacitor.

The ADP320 triple LDO is available in a miniature 16-lead 3 mm × 3 mm LFCSP package and is stable with tiny 1 μF ±30% ceramic output capacitors, resulting in the smallest possible board area for a wide variety of portable power needs.

The ADP320 triple LDO is available in output voltage combinations ranging from 0.8 V to 3.3 V and offers over current and thermal protection to prevent damage in adverse conditions.

## TABLE OF CONTENTS

Features .....	1
Applications.....	1
Typical Application Circuits.....	1
General Description .....	1
Revision History .....	2
Specifications.....	3
Input and Output Capacitor, Recommended Specifications..	4
Absolute Maximum Ratings.....	5
Thermal Resistance .....	5
ESD Caution.....	5
Pin Configurations and Function Descriptions .....	6
Typical Performance Characteristics .....	7

## REVISION HISTORY

### 2/2017—Rev. B to Rev. C

Updated Outline Dimensions .....	21
Changes to Ordering Guide .....	21

### 11/2014—Rev. A to Rev. B

Changes to Features Section.....	1
Changes to Table 1 .....	3
Changes to Figure 28, Figure 29, Figure 30, and Figure 31; Added Figure 32; Renumbered Sequentially .....	11

Theory of Operation .....	15
Applications Information .....	16
ADIsimPower Design Tool .....	16
Capacitor Selection .....	16
Undervoltage Lockout .....	17
Enable Feature .....	17
Current-Limit and Thermal Overload Protection.....	18
Thermal Considerations.....	18
Printed Circuit Board Layout Considerations.....	20
Outline Dimensions .....	21
Ordering Guide .....	21

Added Figure 33 and Figure 34; Changes to Figure 36, Figure 37, and Figure 38 .....	12
Added Figure 39 .....	13
Added ADIsimPower Design Tool Section.....	16

### 4/2011—Rev. 0 to Rev. A

Changes to Ordering Guide .....	20
---------------------------------	----

### 6/2010—Revision 0: Initial Version

## SPECIFICATIONS

$V_{IN1}/V_{IN2} = V_{IN3} = (V_{OUT} + 0.5 \text{ V})$  or 1.8 V (whichever is greater),  $V_{BIAS} = 2.5 \text{ V}$ ,  $EN1, EN2, EN3 = V_{BIAS}$ ,  $I_{OUT1} = I_{OUT2} = I_{OUT3} = 10 \text{ mA}$ ,  $C_{IN} = C_{OUT1} = C_{OUT2} = C_{OUT3} = 1 \mu\text{F}$ , and  $T_A = 25^\circ\text{C}$ , unless otherwise noted.

Table 1.

Parameter	Symbol	Conditions	Min	Typ	Max	Unit	
INPUT BIAS VOLTAGE RANGE	$V_{BIAS}$	$T_J = -40^\circ\text{C}$ to $+125^\circ\text{C}$	2.5		5.5	V	
INPUT LDO VOLTAGE RANGE	$V_{IN1}/V_{IN2}/V_{IN3}$	$T_J = -40^\circ\text{C}$ to $+125^\circ\text{C}$	1.8		5.5	V	
GROUND CURRENT WITH ALL REGULATORS ON	$I_{GND}$	$I_{OUT} = 0 \mu\text{A}$		85		$\mu\text{A}$	
		$I_{OUT} = 0 \mu\text{A}$ , $T_J = -40^\circ\text{C}$ to $+125^\circ\text{C}$			160	$\mu\text{A}$	
		$I_{OUT} = 10 \text{ mA}$		120		$\mu\text{A}$	
		$I_{OUT} = 10 \text{ mA}$ , $T_J = -40^\circ\text{C}$ to $+125^\circ\text{C}$			220	$\mu\text{A}$	
		$I_{OUT} = 200 \text{ mA}$		250		$\mu\text{A}$	
		$I_{OUT} = 200 \text{ mA}$ , $T_J = -40^\circ\text{C}$ to $+125^\circ\text{C}$			380	$\mu\text{A}$	
INPUT BIAS CURRENT	$I_{BIAS}$	$T_J = -40^\circ\text{C}$ to $+125^\circ\text{C}$		66		$\mu\text{A}$	
					140	$\mu\text{A}$	
SHUTDOWN CURRENT	$I_{GND-SD}$	$EN1 = EN2 = EN3 = \text{GND}$		0.1		$\mu\text{A}$	
		$EN1 = EN2 = EN3 = \text{GND}$ , $T_J = -40^\circ\text{C}$ to $+125^\circ\text{C}$			2.5	$\mu\text{A}$	
OUTPUT VOLTAGE ACCURACY	$V_{OUT}$	$100 \mu\text{A} < I_{OUT} < 200 \text{ mA}$ , $V_{IN} = (V_{OUT} + 0.5 \text{ V})$ to 5.5 V, $T_J = -40^\circ\text{C}$ to $+125^\circ\text{C}$	-1		+1	%	
			-2		+2	%	
LINE REGULATION	$\Delta V_{OUT}/\Delta V_{IN}$	$V_{IN} = (V_{OUT} + 0.5 \text{ V})$ to 5.5 V		0.01		%/V	
		$V_{IN} = (V_{OUT} + 0.5 \text{ V})$ to 5.5 V, $T_J = -40^\circ\text{C}$ to $+125^\circ\text{C}$	-0.03		+0.03	%/V	
LOAD REGULATION <sup>1</sup>	$\Delta V_{OUT}/\Delta I_{OUT}$	$I_{OUT} = 1 \text{ mA}$ to 200 mA		0.001		%/mA	
		$I_{OUT} = 1 \text{ mA}$ to 200 mA, $T_J = -40^\circ\text{C}$ to $+125^\circ\text{C}$			0.005	%/mA	
DROPOUT VOLTAGE <sup>2</sup>	$V_{DROPOUT}$	$V_{OUT} = 3.3 \text{ V}$		6		mV	
		$I_{OUT} = 10 \text{ mA}$			9	mV	
		$I_{OUT} = 10 \text{ mA}$ , $T_J = -40^\circ\text{C}$ to $+125^\circ\text{C}$				mV	
		$I_{OUT} = 200 \text{ mA}$		110		mV	
		$I_{OUT} = 200 \text{ mA}$ , $T_J = -40^\circ\text{C}$ to $+125^\circ\text{C}$			170	mV	
START-UP TIME <sup>3</sup>	$T_{START-UP}$	$V_{OUT} = 3.3 \text{ V}$ , all $V_{OUT}$ initially off, enable one		240		$\mu\text{s}$	
		$V_{OUT} = 0.8 \text{ V}$		100		$\mu\text{s}$	
		$V_{OUT} = 3.3 \text{ V}$ , one $V_{OUT}$ initially on, enable second		160		$\mu\text{s}$	
		$V_{OUT} = 0.8 \text{ V}$		20		$\mu\text{s}$	
CURRENT LIMIT THRESHOLD <sup>4</sup>	$I_{LIMIT}$		250	360	600	mA	
THERMAL SHUTDOWN	Thermal Shutdown Threshold Thermal Shutdown Hysteresis	$T_J$ rising $T_{SD-HYS}$		155		$^\circ\text{C}$	
				15		$^\circ\text{C}$	
EN INPUT	EN Input Logic High	$V_{IH}$	$2.5 \text{ V} \leq V_{BIAS} \leq 5.5 \text{ V}$	1.2		V	
	EN Input Logic Low	$V_{IL}$	$2.5 \text{ V} \leq V_{BIAS} \leq 5.5 \text{ V}$		0.4	V	
	EN Input Leakage Current	$V_{I-LEAKAGE}$	$EN1 = EN2 = EN3 = V_{IN}$ or GND $EN1 = EN2 = EN3 = V_{IN}$ or GND, $T_J = -40^\circ\text{C}$ to $+125^\circ\text{C}$		0.1	1	$\mu\text{A}$ $\mu\text{A}$
UNDERVOLTAGE LOCKOUT	Input Bias Voltage (VBIAS) Rising	$UVLO_{RISE}$			2.45	V	
	Input Bias Voltage (VBIAS) Falling	$UVLO_{FALL}$				V	
	Hysteresis	$UVLO_{HYS}$		2.0		180	mV
OUTPUT NOISE	$OUT_{NOISE}$	10 Hz to 100 kHz, $V_{IN} = 5 \text{ V}$ , $V_{OUT} = 3.3 \text{ V}$		50		$\mu\text{V rms}$	
		10 Hz to 100 kHz, $V_{IN} = 5 \text{ V}$ , $V_{OUT} = 2.8 \text{ V}$		43		$\mu\text{V rms}$	
		10 Hz to 100 kHz, $V_{IN} = 3.6 \text{ V}$ , $V_{OUT} = 2.5 \text{ V}$		40		$\mu\text{V rms}$	
		10 Hz to 100 kHz, $V_{IN} = 3.6 \text{ V}$ , $V_{OUT} = 1.2 \text{ V}$		24		$\mu\text{V rms}$	

Parameter	Symbol	Conditions	Min	Typ	Max	Unit		
POWER SUPPLY REJECTION RATIO	PSRR	$V_{IN} = 1.8\text{ V}$ , $V_{OUT} = 0.8\text{ V}$ , $I_{OUT} = 100\text{ mA}$						
			100 Hz		70		dB	
			1 kHz		70		dB	
			10 kHz		70		dB	
			100 kHz		60		dB	
			1 MHz		40		dB	
		$V_{IN} = 3.3\text{ V}$ , $V_{OUT} = 2.8\text{ V}$ , $I_{OUT} = 100\text{ mA}$						
			100 Hz		68		dB	
			1 kHz		62		dB	
			10 kHz		68		dB	
			100 kHz		60		dB	
			1 MHz		40		dB	

<sup>1</sup> Based on an end-point calculation using 1 mA and 200 mA loads.

<sup>2</sup> Dropout voltage is defined as the input-to-output voltage differential when the input voltage is set to the nominal output voltage. This applies only for output voltages above 1.8 V.

<sup>3</sup> Start-up time is defined as the time between the rising edge of ENx to  $V_{OUTx}$  being at 90% of its nominal value.

<sup>4</sup> Current-limit threshold is defined as the current at which the output voltage drops to 90% of the specified typical value. For example, the current limit for a 3.0 V output voltage is defined as the current that causes the output voltage to drop to 90% of 3.0 V, or 2.7 V.

## INPUT AND OUTPUT CAPACITOR, RECOMMENDED SPECIFICATIONS

Table 2.

Parameter	Symbol	Conditions	Min	Typ	Max	Unit
MINIMUM INPUT AND OUTPUT CAPACITANCE <sup>1</sup>	$C_{MIN}$	$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$	0.70			$\mu\text{F}$
CAPACITOR ESR	$R_{ESR}$	$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$	0.001		1	$\Omega$

<sup>1</sup> The minimum input and output capacitance must be greater than 0.70  $\mu\text{F}$  over the full range of operating conditions. The full range of operating conditions in the application must be considered during device selection to ensure that the minimum capacitance specification is met. X7R and X5R type capacitors are recommended, Y5V and Z5U capacitors are not recommended for use with LDOs.

## ABSOLUTE MAXIMUM RATINGS

Table 3.

Parameter	Rating
VIN1/VIN2, VIN3, VBIAS to GND	-0.3 V to +6.5 V
VOUT1, VOUT2 to GND	-0.3 V to VIN1/VIN2
VOUT3 to GND	-0.3 V to VIN3
EN1, EN2, EN3 to GND	-0.3 V to +6.5 V
Storage Temperature Range	-65°C to +150°C
Operating Junction Temperature Range	-40°C to +125°C
Soldering Conditions	JEDEC J-STD-020

Stresses at or above those listed under Absolute Maximum Ratings may cause permanent damage to the product. This is a stress rating only; functional operation of the product at these or any other conditions above those indicated in the operational section of this specification is not implied. Operation beyond the maximum operating conditions for extended periods may affect product reliability.

### THERMAL DATA

Absolute maximum ratings apply individually only, not in combination.

The ADP320 triple LDO can be damaged when the junction temperature limits are exceeded. Monitoring ambient temperature does not guarantee that the junction temperature ( $T_J$ ) is within the specified temperature limits. In applications with high power dissipation and poor thermal resistance the maximum ambient temperature may have to be derated. In applications with moderate power dissipation and low PCB thermal resistance, the maximum ambient temperature can exceed the maximum limit as long as the junction temperature is within specification limits.

The junction temperature ( $T_J$ ) of the device is dependent on the ambient temperature ( $T_A$ ), the power dissipation of the device ( $P_D$ ), and the junction-to-ambient thermal resistance of the package ( $\theta_{JA}$ ). Maximum junction temperature ( $T_J$ ) is calculated from the ambient temperature ( $T_A$ ) and power dissipation ( $P_D$ ) using the following formula:

$$T_J = T_A + (P_D \times \theta_{JA})$$

Junction-to-ambient thermal resistance ( $\theta_{JA}$ ) of the package is based on modeling and calculation using a 4-layer board. The junction-to-ambient thermal resistance is highly dependent on the application and board layout. In applications where high maximum power dissipation exists, close attention to thermal board design is required. The value of  $\theta_{JA}$  may vary, depending on PCB material, layout, and environmental conditions. The specified values of  $\theta_{JA}$  are based on a four-layer, 4-inch  $\times$  3-inch circuit board. Refer to JEDEC JESD 51-9 for detailed information on the board construction. For additional information, see the AN-617 Application Note, *MicroCSP™ Wafer Level Chip Scale Package*.

$\Psi_{JB}$  is the junction to board thermal characterization parameter with units of °C/W.  $\Psi_{JB}$  of the package is based on modeling and calculation using a 4-layer board. The JESD51-12, *Guidelines for Reporting and Using Package Thermal Information*, states that thermal characterization parameters are not the same as thermal resistances.  $\Psi_{JB}$  measures the component power flowing through multiple thermal paths rather than a single path as in thermal resistance,  $\theta_{JB}$ . Therefore,  $\Psi_{JB}$  thermal paths include convection from the top of the package as well as radiation from the package; factors that make  $\Psi_{JB}$  more useful in real-world applications. Maximum junction temperature ( $T_J$ ) is calculated from the board temperature ( $T_B$ ) and power dissipation ( $P_D$ ) using the following formula

$$T_J = T_B + (P_D \times \Psi_{JB})$$

Refer to JEDEC JESD51-8 and JESD51-12 for more detailed information about  $\Psi_{JB}$ .

### THERMAL RESISTANCE

$\theta_{JA}$  and  $\Psi_{JB}$  are specified for the worst-case conditions, that is, a device soldered in a circuit board for surface-mount packages.

Table 4.

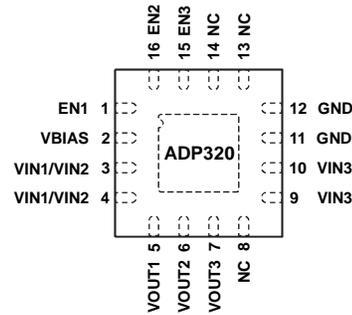
Package Type	$\theta_{JA}$	$\Psi_{JB}$	Unit
16-Lead 3 mm $\times$ 3 mm LFCSP	49.5	25.2	°C/W

### ESD CAUTION



**ESD (electrostatic discharge) sensitive device.** Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD. Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

## PIN CONFIGURATIONS AND FUNCTION DESCRIPTIONS

TOP VIEW  
(Not to Scale)

## NOTES

1. NC = NO CONNECT.
2. CONNECT EXPOSED PAD TO GROUND PLANE.

09874-002

Figure 2. Pin Configuration

Table 5. Pin Function Descriptions

Pin No.	Mnemonic	Description
1	EN1	Enable Input for Regulator 1. Drive EN1 high to turn on Regulator 1; drive it low to turn off Regulator 1. For automatic startup, connect EN1 to VBIAS.
2	VBIAS	Input Voltage Bias Supply. Bypass VBIAS to GND with a 1 $\mu$ F or greater capacitor.
3	VIN1/VIN2	Regulator Input Supply for Output Voltage 1 and Output Voltage 2. Bypass VIN1/VIN2 to GND with a 1 $\mu$ F or greater capacitor.
4	VIN1/VIN2	Regulator Input Supply for Output Voltage 1 and Output Voltage 2. Bypass VIN1/VIN2 to GND with a 1 $\mu$ F or greater capacitor.
5	VOUT1	Regulated Output Voltage 1. Connect a 1 $\mu$ F or greater output capacitor between VOUT1 and GND.
6	VOUT2	Regulated Output Voltage 2. Connect a 1 $\mu$ F or greater output capacitor between VOUT2 and GND.
7	VOUT3	Regulated Output Voltage 3. Connect a 1 $\mu$ F or greater output capacitor between VOUT3 and GND.
8	NC	Not connected internally.
9	VIN3	Regulator Input Supply for Output Voltage 3. Bypass VIN3 to GND with a 1 $\mu$ F or greater capacitor.
10	VIN3	Regulator Input Supply for Output Voltage 3. Bypass VIN3 to GND with a 1 $\mu$ F or greater capacitor.
11	GND	Ground Pin.
12	GND	Ground Pin.
13	NC	Not connected internally.
14	NC	Not connected internally.
15	EN3	Enable Input for Regulator 3. Drive EN3 high to turn on Regulator 3; drive it low to turn off Regulator 3. For automatic startup, connect EN3 to VBIAS.
16	EN2	Enable Input for Regulator 2. Drive EN2 high to turn on Regulator 2; drive it low to turn off Regulator 2. For automatic startup, connect EN2 to VBIAS.
EP	EP	Exposed pad for enhanced thermal performance. Connect to copper ground plane.

### TYPICAL PERFORMANCE CHARACTERISTICS

$V_{IN1}/V_{IN2} = V_{IN3} = V_{BIAS} = 4\text{ V}$ ,  $V_{OUT1} = 3.3\text{ V}$ ,  $V_{OUT2} = 1.8\text{ V}$ ,  $V_{OUT3} = 1.5\text{ V}$ ,  $I_{OUT} = 10\text{ mA}$ ,  $C_{IN} = C_{OUT1} = C_{OUT2} = C_{OUT3} = 1\text{ }\mu\text{F}$ ,  $T_A = 25^\circ\text{C}$ , unless otherwise noted.

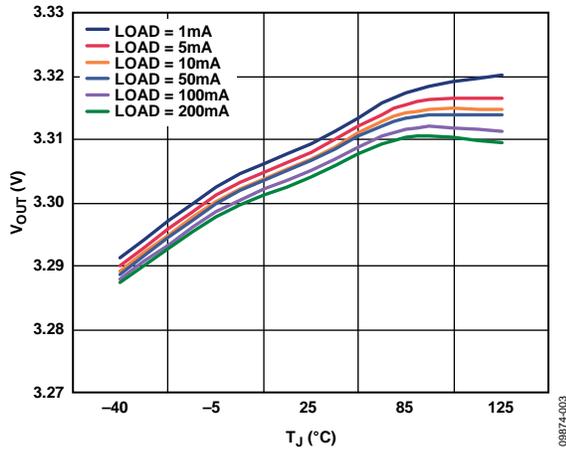


Figure 3. Output Voltage vs. Junction Temperature,  $V_{RIPPLE} = 50\text{ mV}$ ,  $C_{OUT} = 1\text{ }\mu\text{F}$

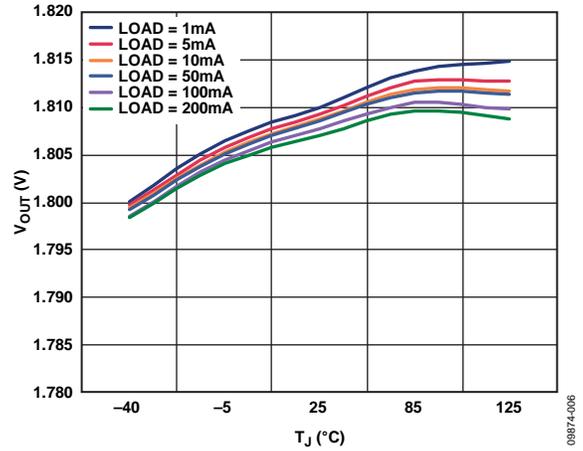


Figure 6. Output Voltage vs. Junction Temperature,  $V_{RIPPLE} = 50\text{ mV}$ ,  $C_{OUT} = 1\text{ }\mu\text{F}$

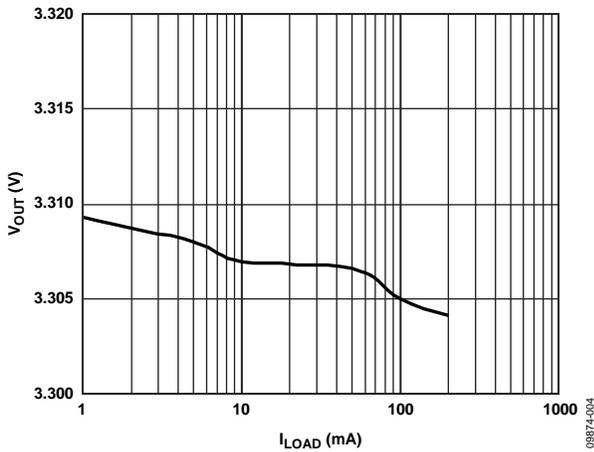


Figure 4. Output Voltage vs. Load Current,  $V_{RIPPLE} = 50\text{ mV}$ ,  $C_{OUT} = 1\text{ }\mu\text{F}$

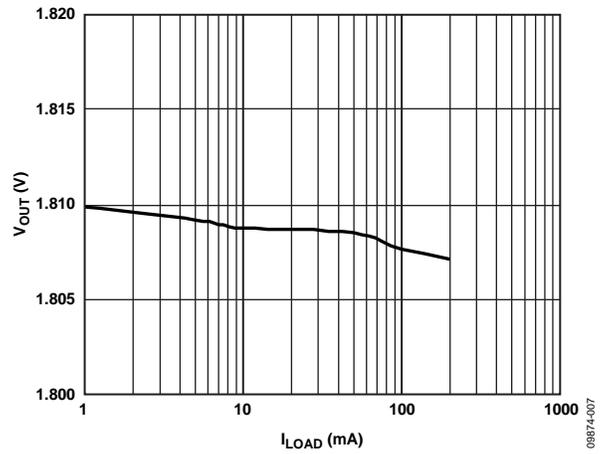


Figure 7. Output Voltage vs. Load Current,  $V_{RIPPLE} = 50\text{ mV}$ ,  $C_{OUT} = 1\text{ }\mu\text{F}$

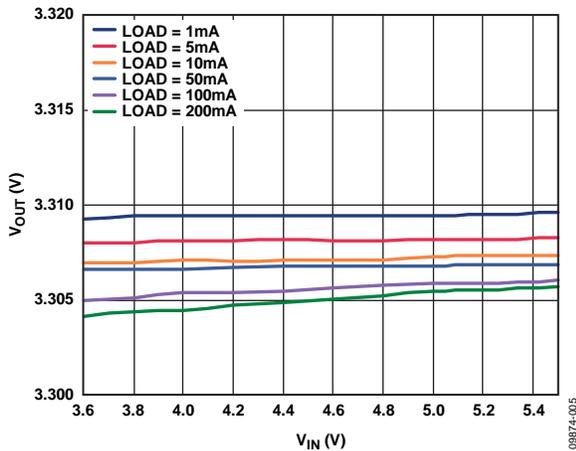


Figure 5. Output Voltage vs. Input Voltage,  $V_{RIPPLE} = 50\text{ mV}$ ,  $C_{OUT} = 1\text{ }\mu\text{F}$

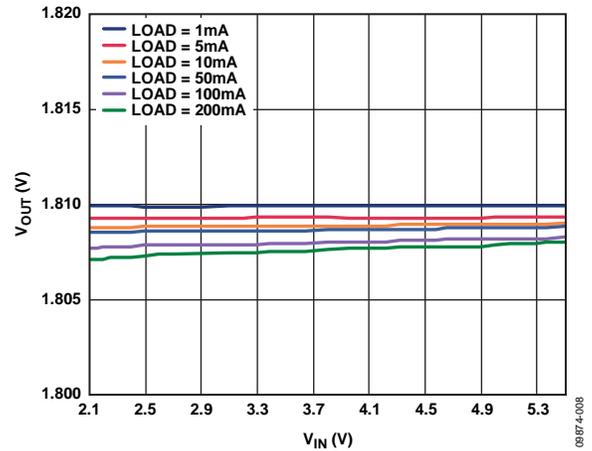


Figure 8. Output Voltage vs. Input Voltage,  $V_{RIPPLE} = 50\text{ mV}$ ,  $C_{OUT} = 1\text{ }\mu\text{F}$

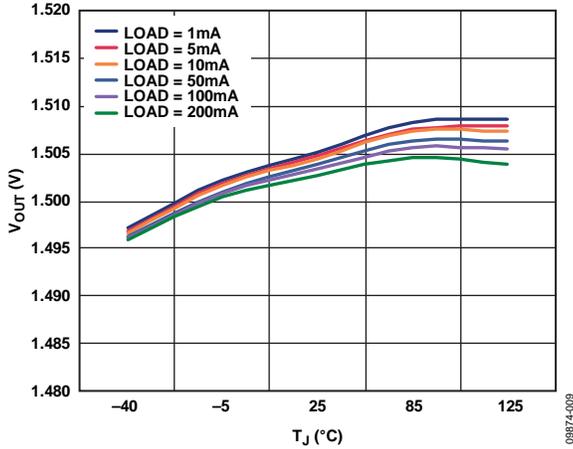


Figure 9. Output Voltage vs. Junction Temperature,  $V_{RIPPLE} = 50\text{ mV}$ ,  $C_{OUT} = 1\ \mu\text{F}$

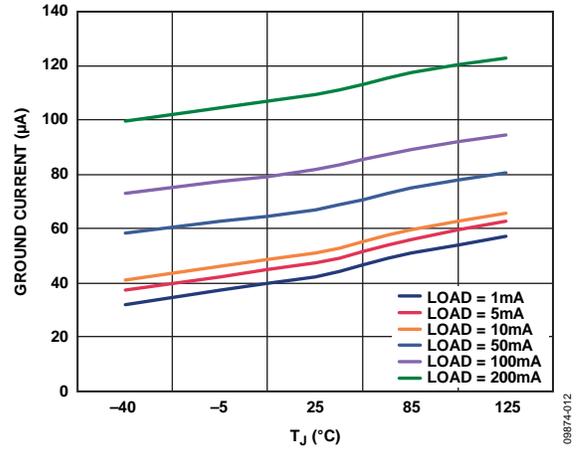


Figure 12. Ground Current vs. Junction Temperature, Single Output Loaded,  $V_{RIPPLE} = 50\text{ mV}$ ,  $C_{OUT} = 1\ \mu\text{F}$

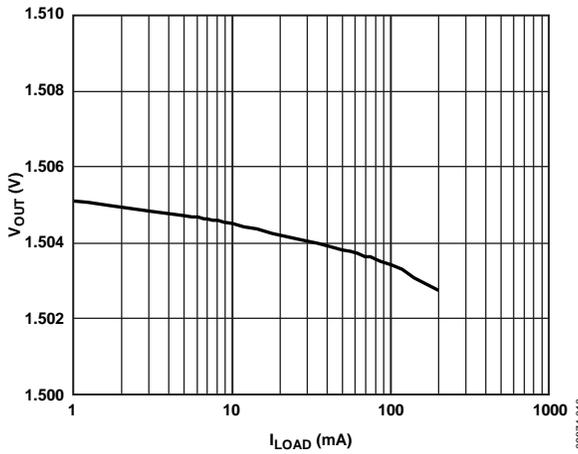


Figure 10. Output Voltage vs. Load Current,  $V_{RIPPLE} = 50\text{ mV}$ ,  $C_{OUT} = 1\ \mu\text{F}$

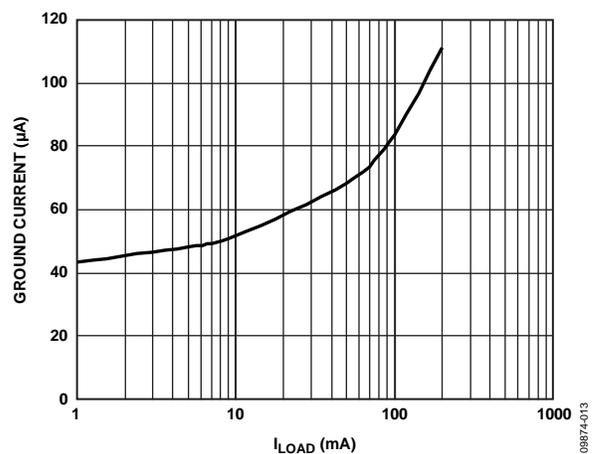


Figure 13. Ground Current vs. Load Current, Single Output Loaded,  $V_{RIPPLE} = 50\text{ mV}$ ,  $C_{OUT} = 1\ \mu\text{F}$

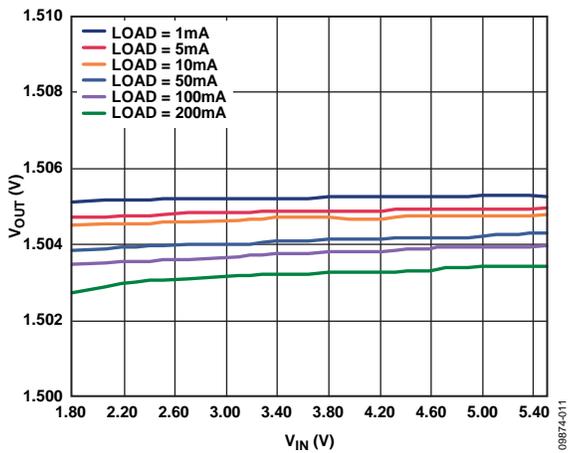


Figure 11. Output Voltage vs. Input Voltage,  $V_{RIPPLE} = 50\text{ mV}$ ,  $C_{OUT} = 1\ \mu\text{F}$

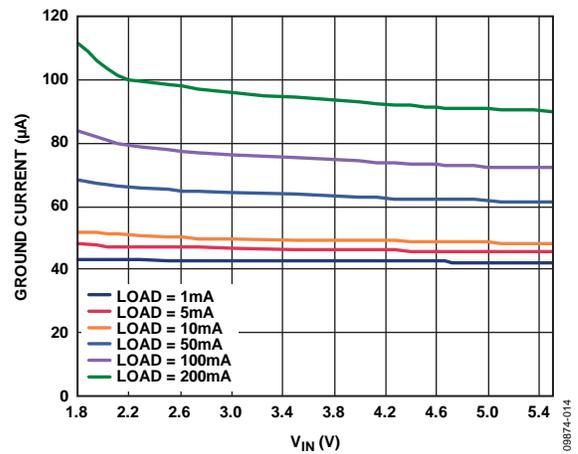


Figure 14. Ground Current vs. Input Voltage, Single Output Loaded,  $V_{RIPPLE} = 50\text{ mV}$ ,  $C_{OUT} = 1\ \mu\text{F}$

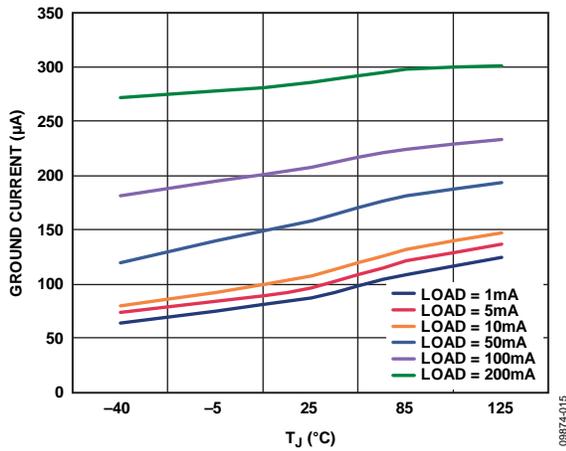


Figure 15. Ground Current vs. Junction Temperature, All Outputs Loaded Equally,  $V_{RIPPLE} = 50\text{ mV}$ ,  $C_{OUT} = 1\text{ }\mu\text{F}$

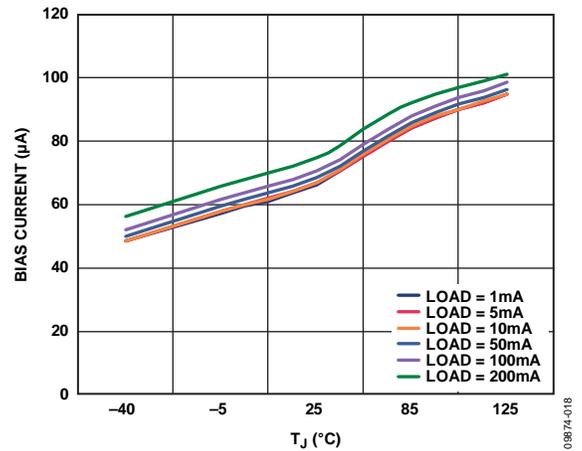


Figure 18. Bias Current vs. Junction Temperature, Single Output Loaded,  $V_{RIPPLE} = 50\text{ mV}$ ,  $C_{OUT} = 1\text{ }\mu\text{F}$

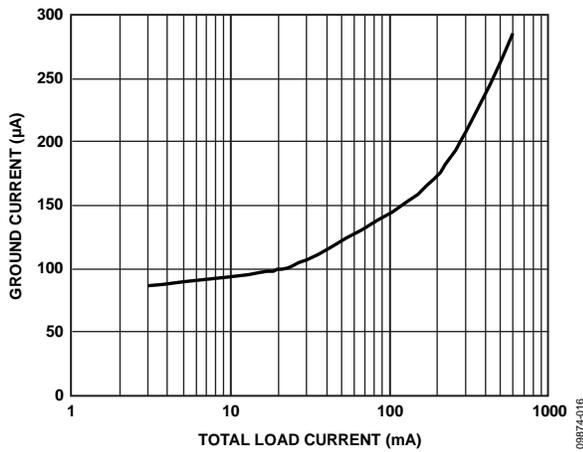


Figure 16. Ground Current vs. Load Current, All Outputs Loaded Equally,  $V_{RIPPLE} = 50\text{ mV}$ ,  $C_{OUT} = 1\text{ }\mu\text{F}$

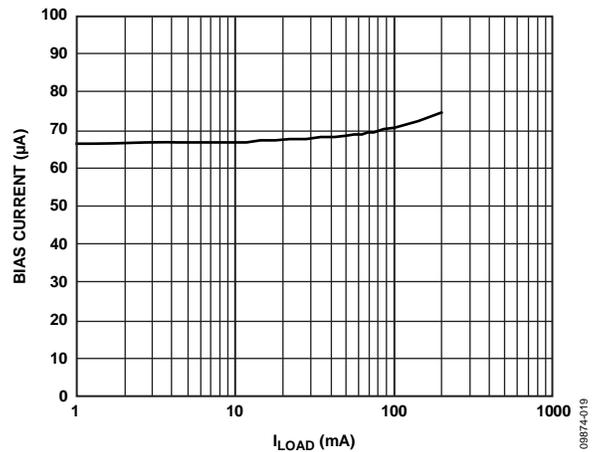


Figure 19. Bias Current vs. Load Current, Single Output Load,  $V_{RIPPLE} = 50\text{ mV}$ ,  $C_{OUT} = 1\text{ }\mu\text{F}$

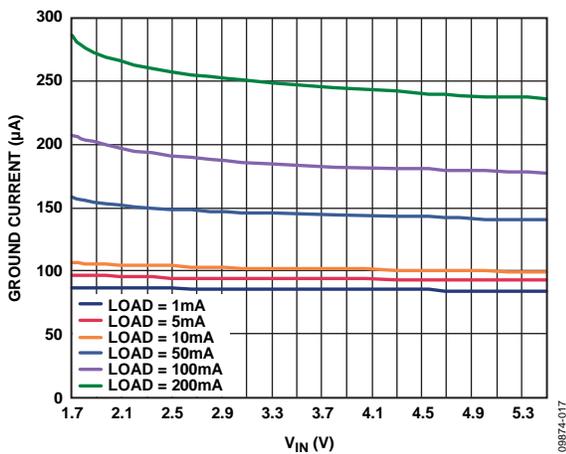


Figure 17. Ground Current vs. Input Voltage, All Outputs Loaded Equally,  $V_{RIPPLE} = 50\text{ mV}$ ,  $C_{OUT} = 1\text{ }\mu\text{F}$

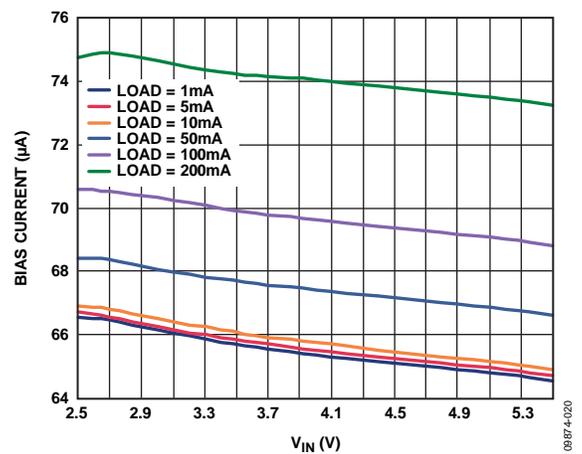


Figure 20. Bias Current vs. Input Voltage, Single Output Load,  $V_{RIPPLE} = 50\text{ mV}$ ,  $C_{OUT} = 1\text{ }\mu\text{F}$

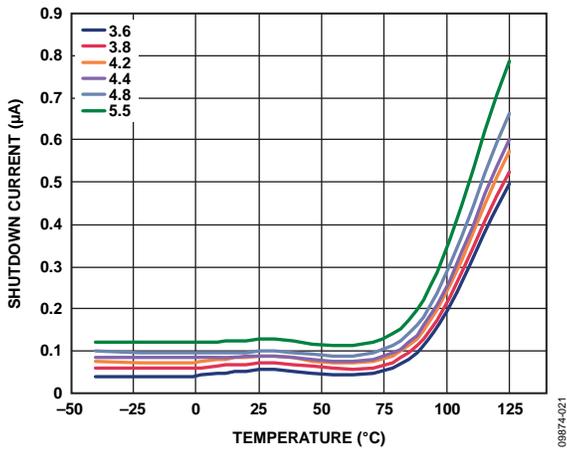


Figure 21. Shutdown Current vs. Temperature at Various Input Voltages,  $V_{RIPPLE} = 50\text{ mV}$ ,  $C_{OUT} = 1\text{ }\mu\text{F}$

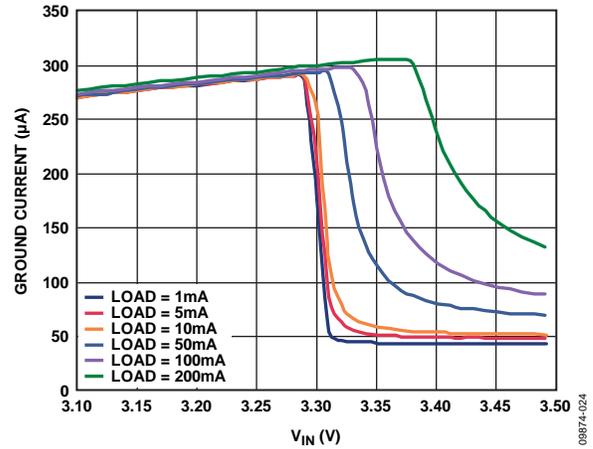


Figure 24. Ground Current vs. Input Voltage (in Dropout),  $V_{OUT1} = 3.3\text{ V}$ ,  $V_{RIPPLE} = 50\text{ mV}$ ,  $C_{OUT} = 1\text{ }\mu\text{F}$

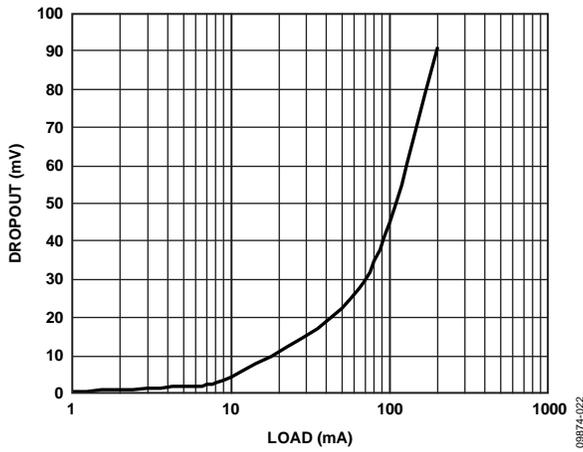


Figure 22. Dropout Voltage vs. Load Current and Output Voltage,  $V_{OUT1} = 3.3\text{ V}$ ,  $V_{RIPPLE} = 50\text{ mV}$ ,  $C_{OUT} = 1\text{ }\mu\text{F}$

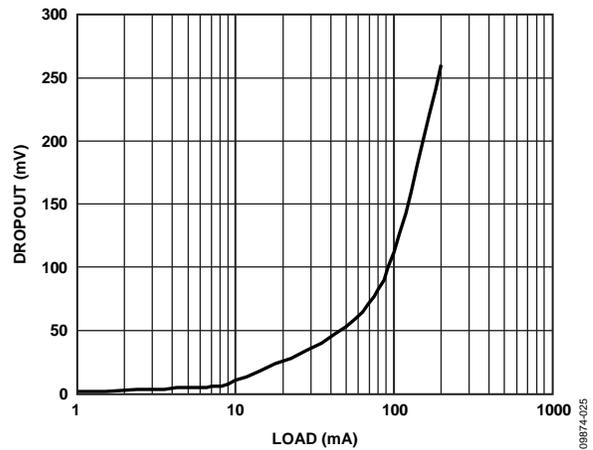


Figure 25. Dropout Voltage vs. Load Current and Output Voltage,  $V_{OUT2} = 1.8\text{ V}$ ,  $V_{RIPPLE} = 50\text{ mV}$ ,  $C_{OUT} = 1\text{ }\mu\text{F}$

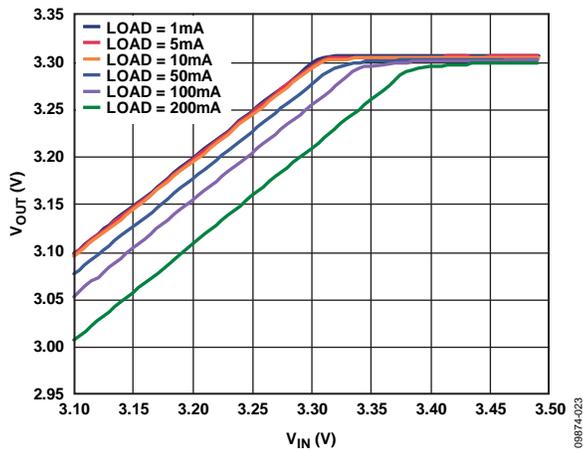


Figure 23. Output Voltage vs. Input Voltage (In Dropout),  $V_{OUT1} = 3.3\text{ V}$ ,  $V_{RIPPLE} = 50\text{ mV}$ ,  $C_{OUT} = 1\text{ }\mu\text{F}$

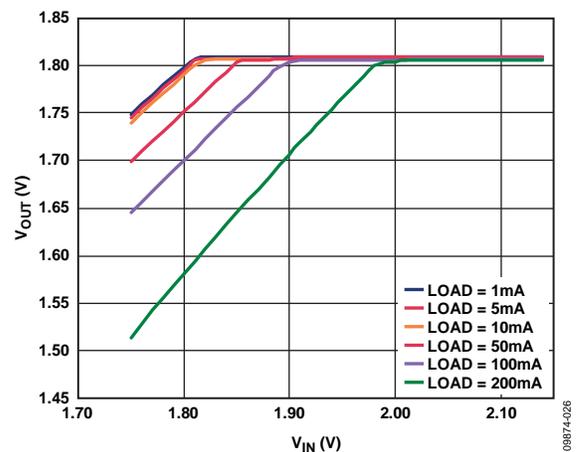


Figure 26. Output Voltage vs. Input Voltage (in Dropout),  $V_{OUT2} = 1.8\text{ V}$ ,  $V_{RIPPLE} = 50\text{ mV}$ ,  $C_{OUT} = 1\text{ }\mu\text{F}$

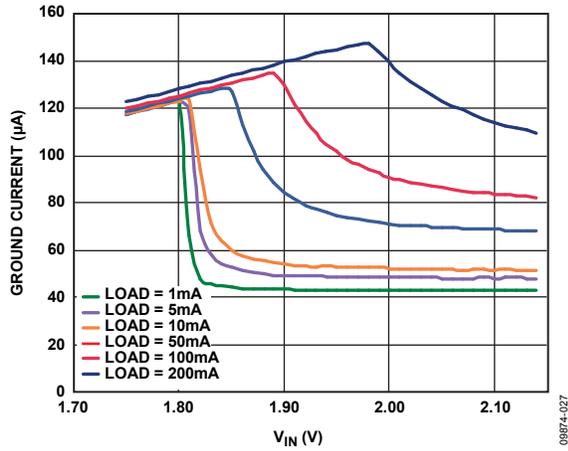


Figure 27. Ground Current vs. Input Voltage in Dropout,  $V_{OUT2} = 1.8 V$ ,  $V_{RIPPLE} = 50 mV$ ,  $C_{OUT} = 1 \mu F$

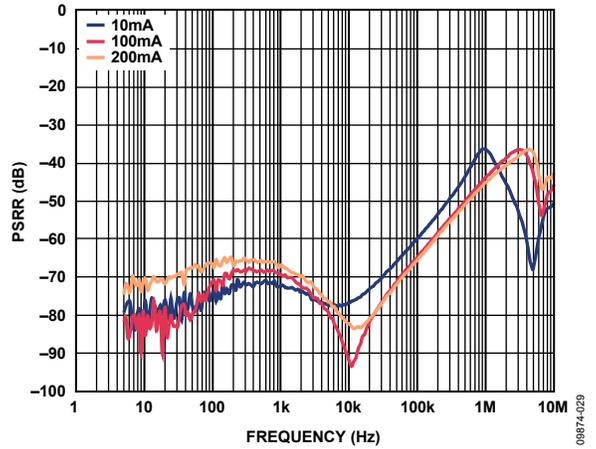


Figure 30. Power Supply Rejection Ratio vs. Frequency,  $V_{OUT} = 3.3 V$ ,  $V_{IN} = 4.3 V$ ,  $V_{RIPPLE} = 50 mV$ ,  $C_{OUT} = 1 \mu F$

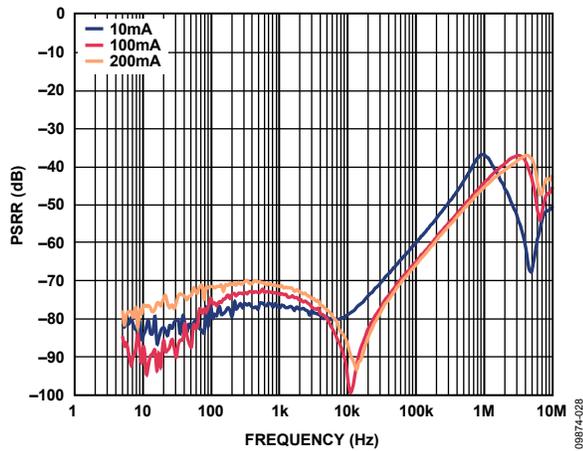


Figure 28. Power Supply Rejection Ratio vs. Frequency,  $V_{OUT} = 1.8 V$ ,  $V_{IN} = 2.8 V$ ,  $V_{RIPPLE} = 50 mV$ ,  $C_{OUT} = 1 \mu F$

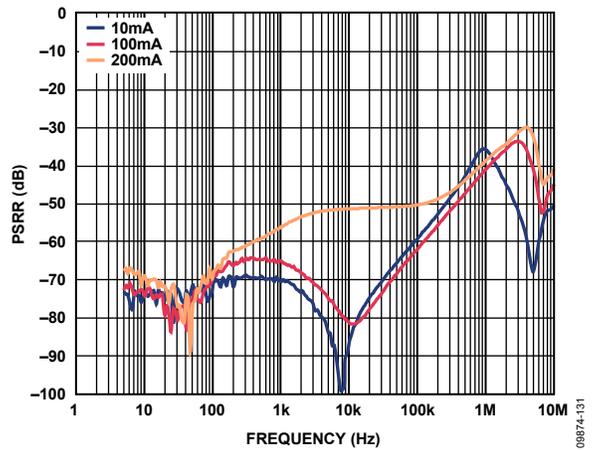


Figure 31. Power Supply Rejection Ratio vs. Frequency,  $V_{OUT} = 3.3 V$ ,  $V_{IN} = 3.8 V$ ,  $V_{RIPPLE} = 50 mV$ ,  $C_{OUT} = 1 \mu F$

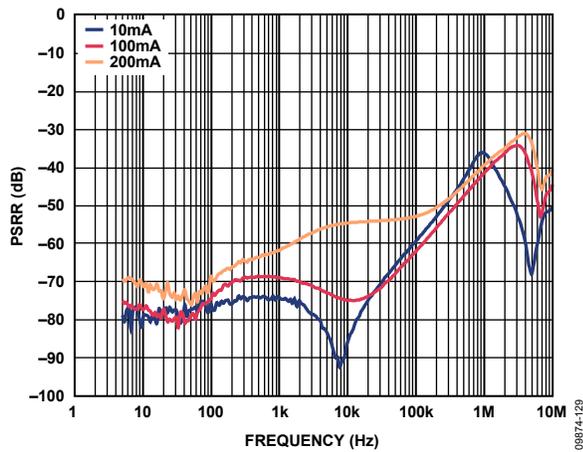


Figure 29. Power Supply Rejection Ratio vs. Frequency,  $V_{OUT} = 1.8 V$ ,  $V_{IN} = 2.3 V$ ,  $V_{RIPPLE} = 50 mV$ ,  $C_{OUT} = 1 \mu F$

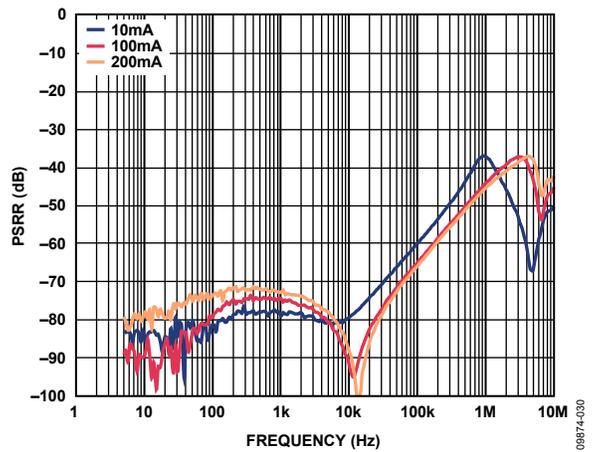


Figure 32. Power Supply Rejection Ratio vs. Frequency,  $V_{OUT} = 1.5 V$ ,  $V_{IN} = 2.5 V$ ,  $V_{RIPPLE} = 50 mV$ ,  $C_{OUT} = 1 \mu F$

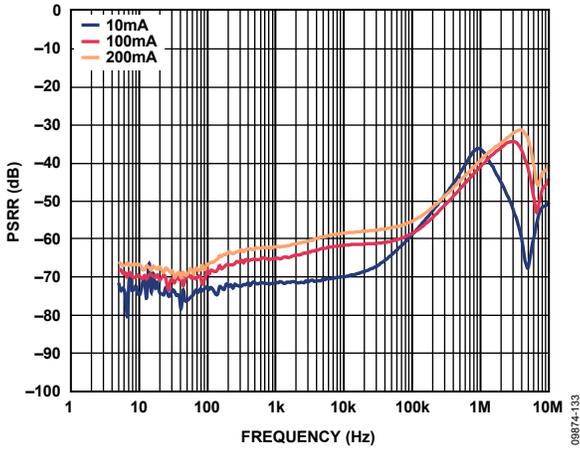


Figure 33. Power Supply Rejection Ratio vs. Frequency,  $V_{OUT} = 1.5 V$ ,  $V_{IN} = 2.0 V$ ,  $V_{RIPPLE} = 50 mV$ ,  $C_{OUT} = 1 \mu F$

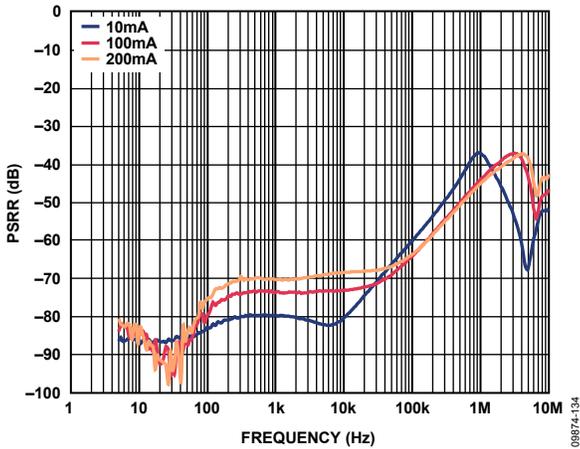


Figure 34. Power Supply Rejection Ratio vs. Frequency,  $V_{OUT} = 1.2 V$ ,  $V_{IN} = 2.2 V$ ,  $V_{RIPPLE} = 50 mV$ ,  $C_{OUT} = 1 \mu F$

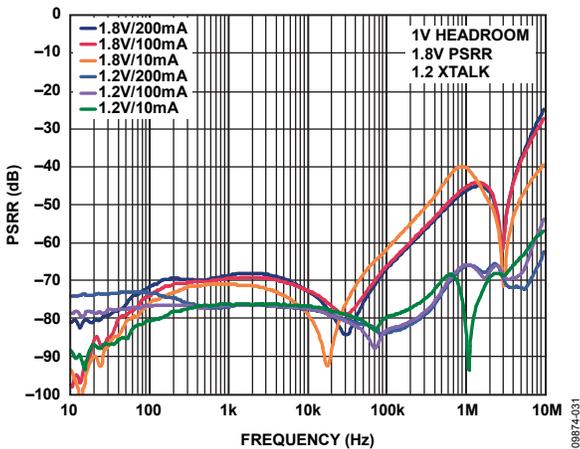


Figure 35. Power Supply Rejection Ratio vs. Frequency, Channel to Channel Crosstalk,  $V_{RIPPLE} = 50 mV$ ,  $C_{OUT} = 1 \mu F$

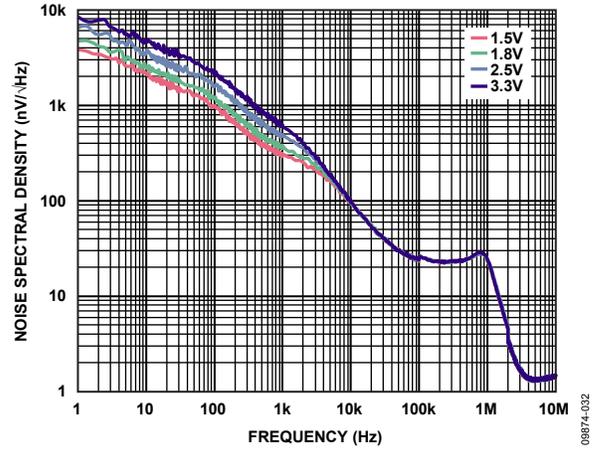


Figure 36. Output Noise Spectral Density,  $V_{IN} = 5 V$ ,  $I_{LOAD} = 10 mA$ ,  $V_{RIPPLE} = 50 mV$ ,  $C_{OUT} = 1 \mu F$

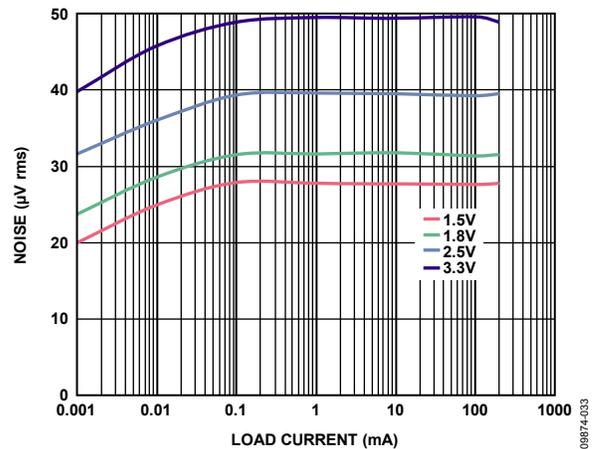


Figure 37. 10 Hz to 100 kHz Output Noise vs. Load Current and Output Voltage,  $V_{IN} = 5 V$ ,  $V_{RIPPLE} = 50 mV$ ,  $C_{OUT} = 1 \mu F$

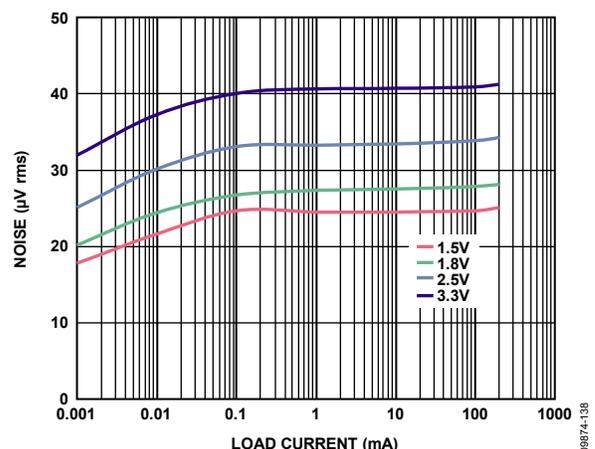


Figure 38. 100 Hz to 100 kHz Output Noise vs. Load Current and Output Voltage,  $V_{IN} = 5 V$ ,  $V_{RIPPLE} = 50 mV$ ,  $C_{OUT} = 1 \mu F$

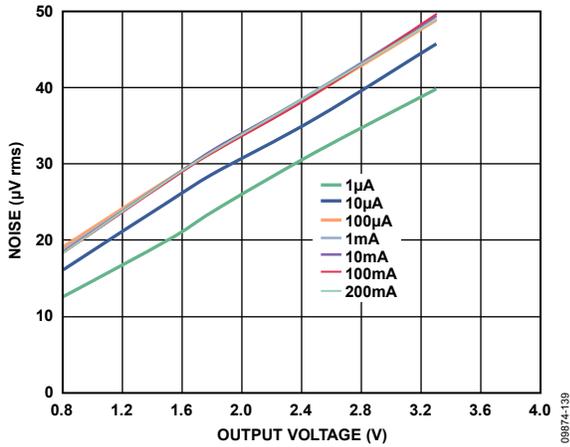


Figure 39. Output Noise vs. Output Voltage, Different Load Currents,  $V_{IN} = 5V$ ,  $V_{RIPPLE} = 50mV$ ,  $C_{OUT} = 1\mu F$

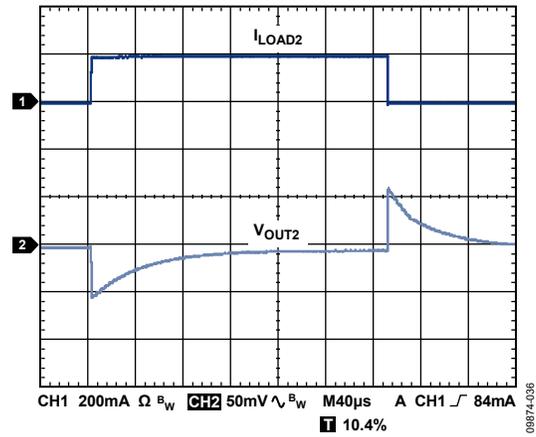


Figure 42. Load Transient Response,  $I_{LOAD2} = 1mA$  to  $200mA$ ,  $C_{OUT2} = 1\mu F$ ,  $CH1 = I_{LOAD2}$ ,  $CH2 = V_{OUT2}$ ,  $V_{RIPPLE} = 50mV$ ,  $C_{OUT} = 1\mu F$

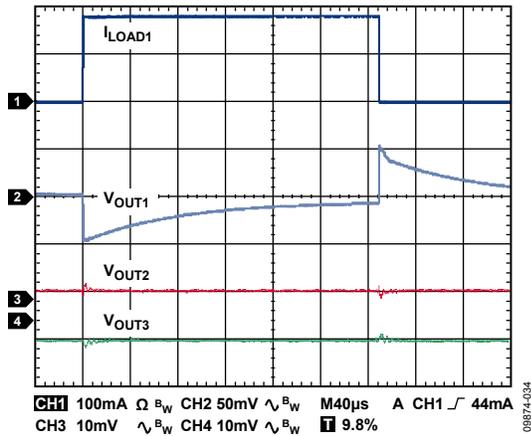


Figure 40. Load Transient Response,  $I_{LOAD1} = 1mA$  to  $200mA$ ,  $I_{LOAD2} = I_{LOAD3} = 1mA$ ,  $CH1 = I_{LOAD1}$ ,  $CH2 = V_{OUT1}$ ,  $CH3 = V_{OUT2}$ ,  $CH4 = V_{OUT3}$ ,  $V_{RIPPLE} = 50mV$ ,  $C_{OUT} = 1\mu F$

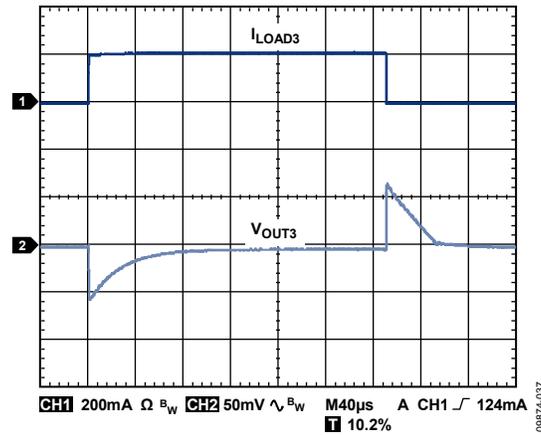


Figure 43. Load Transient Response,  $I_{LOAD3} = 1mA$  to  $200mA$ ,  $C_{OUT3} = 1\mu F$ ,  $CH1 = I_{LOAD3}$ ,  $CH2 = V_{OUT3}$ ,  $V_{RIPPLE} = 50mV$ ,  $C_{OUT} = 1\mu F$

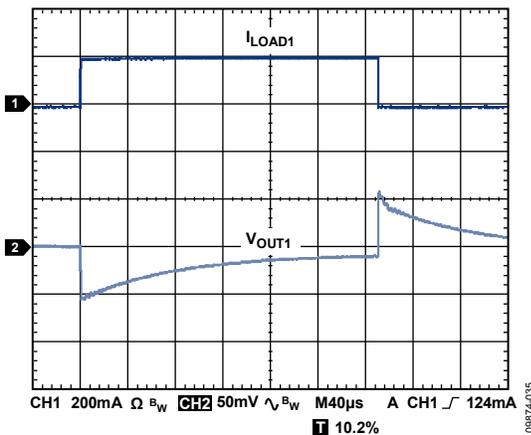


Figure 41. Load Transient Response,  $I_{LOAD1} = 1mA$  to  $200mA$ ,  $C_{OUT1} = 1\mu F$ ,  $CH1 = I_{LOAD1}$ ,  $CH2 = V_{OUT1}$ ,  $V_{RIPPLE} = 50mV$ ,  $C_{OUT} = 1\mu F$

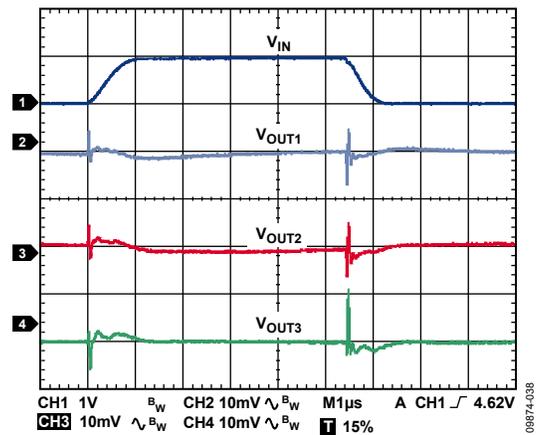


Figure 44. Line Transient Response,  $V_{IN} = 4V$  to  $5V$ ,  $I_{LOAD1} = I_{LOAD2} = I_{LOAD3} = 100mA$ ,  $CH1 = V_{IN}$ ,  $CH2 = V_{OUT1}$ ,  $CH3 = V_{OUT2}$ ,  $CH4 = V_{OUT3}$ ,  $V_{RIPPLE} = 50mV$ ,  $C_{OUT} = 1\mu F$

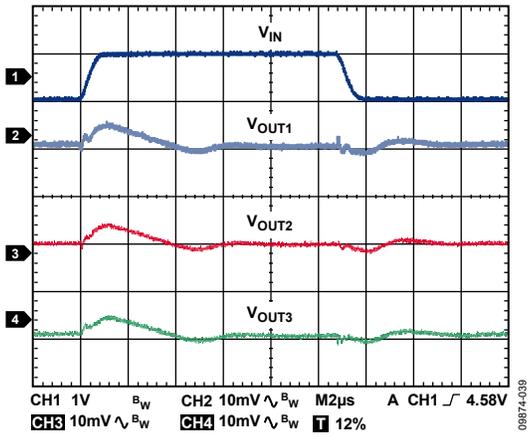


Figure 45. Line Transient Response,  
 $V_{IN} = 4\text{ V to }5\text{ V}$ ,  $I_{LOAD1} = I_{LOAD2} = I_{LOAD3} = 1\text{ mA}$ ,  
 $CH1 = V_{IN}$ ,  $CH2 = V_{OUT1}$ ,  $CH3 = V_{OUT2}$ ,  $CH4 = V_{OUT3}$ ,  
 $V_{RIPPLE} = 50\text{ mV}$ ,  $C_{OUT} = 1\text{ }\mu\text{F}$

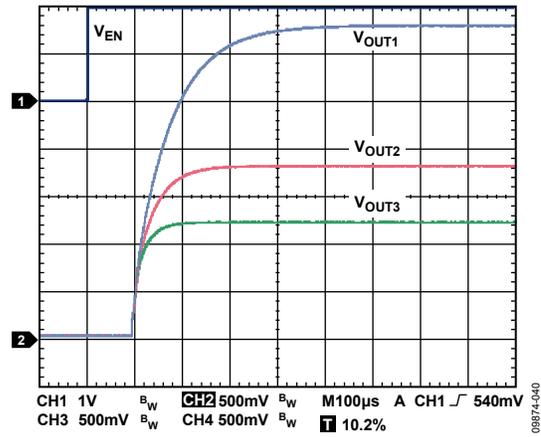


Figure 46. Turn On Response,  
 $I_{LOAD1} = I_{LOAD2} = I_{LOAD3} = 100\text{ mA}$ ,  
 $CH1 = V_{EN}$ ,  $CH2 = V_{OUT1}$ ,  $CH3 = V_{OUT2}$ ,  $CH4 = V_{OUT3}$ ,  
 $V_{RIPPLE} = 50\text{ mV}$ ,  $C_{OUT} = 1\text{ }\mu\text{F}$

## THEORY OF OPERATION

The **ADP320** triple LDO is a low quiescent current, low dropout linear regulator that operates from 1.8 V to 5.5 V on VIN1/VIN2 and VIN3 and provides up to 200 mA of current from each output. Drawing a low 250  $\mu$ A quiescent current (typical) at full load makes the **ADP320** triple LDO ideal for battery-operated portable equipment. Shutdown current consumption is typically 100 nA.

Optimized for use with small 1  $\mu$ F ceramic capacitors, the **ADP320** triple LDO provides excellent transient performance.

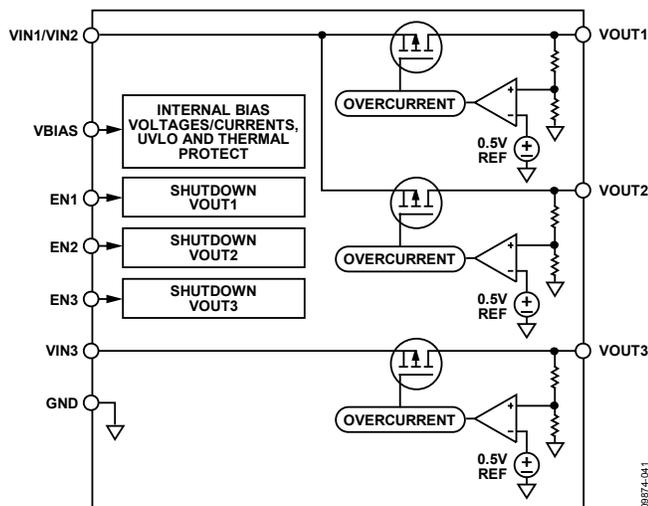


Figure 47. Internal Block Diagram

Internally, the **ADP320** triple LDO consists of a reference, three error amplifiers, three feedback voltage dividers, and three PMOS pass transistors. Output current is delivered via the PMOS pass device, which is controlled by the error amplifier. The error amplifier compares the reference voltage with the feedback voltage from the output and amplifies the difference. If the feedback voltage is lower than the reference voltage, the gate of the PMOS device is pulled lower, allowing more current to flow and increasing the output voltage. If the feedback voltage is higher than the reference voltage, the gate of the PMOS device is pulled higher, allowing less current to flow and decreasing the output voltage.

The **ADP320** triple LDO is available in multiple output voltage options ranging from 0.8 V to 3.3 V. The **ADP320** triple LDO uses the EN1, EN2, and EN3 enable pins to enable and disable the VOUT1/VOUT2/VOUT3 pins under normal operating conditions. When the enable pins are high, VOUT1/VOUT2/VOUT3 turn on; when enable pins are low, VOUT1/VOUT2/VOUT3 turn off. For automatic startup, the enable pins can be tied to VBIAS.

## APPLICATIONS INFORMATION

### ADIsimPOWER DESIGN TOOL

The ADP323 is supported by the ADIsimPower™ design tool set. ADIsimPower is a collection of tools that produce complete power designs optimized for a specific design goal. The tools enable the user to generate a full schematic, bill of materials, and calculate performance in minutes. ADIsimPower can optimize designs for cost, area, efficiency, and parts count, taking into consideration the operating conditions and limitations of the IC and all real external components. For more information about, and to obtain ADIsimPower design tools, visit [www.analog.com/ADIsimPower](http://www.analog.com/ADIsimPower).

### CAPACITOR SELECTION

#### Output Capacitor

The ADP320 triple LDO is designed for operation with small, space-saving ceramic capacitors, but the parts function with most commonly used capacitors as long as care is taken in regards to the effective series resistance (ESR) value. The ESR of the output capacitor affects stability of the LDO control loop. A minimum of 0.70  $\mu\text{F}$  capacitance with an ESR of 1  $\Omega$  or less is recommended to ensure stability of the ADP320 triple LDO. Transient response to changes in load current is also affected by output capacitance. Using a larger value of output capacitance improves the transient response of the ADP320 triple LDO to large changes in the load current. Figure 48 show the transient response for an output capacitance value of 1  $\mu\text{F}$ .

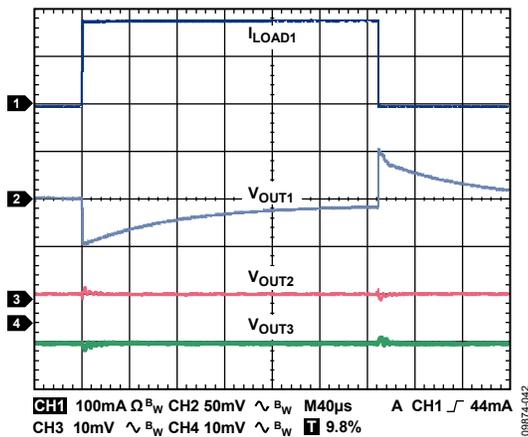


Figure 48. Output Transient Response,  
 $I_{LOAD1} = 1 \text{ mA}$  to  $200 \text{ mA}$ ,  $I_{LOAD2} = 1 \text{ mA}$ ,  $I_{LOAD3} = 1 \text{ mA}$ ,  
 $CH1 = I_{LOAD1}$ ,  $CH2 = V_{OUT1}$ ,  $CH3 = V_{OUT2}$ ,  $CH4 = V_{OUT3}$

#### Input Bypass Capacitor

Connecting a 1  $\mu\text{F}$  capacitor from VIN1/VIN2, VIN3, and VBIAS to GND reduces the circuit sensitivity to the PCB layout, especially when long input traces or high source impedance are encountered. If an output capacitance greater than 1  $\mu\text{F}$  is required, the input capacitor can be increased to match it.

#### Input and Output Capacitor Properties

Any good quality ceramic capacitor may be used with the ADP320 triple LDO, as long as the capacitor meets the minimum capacitance and maximum ESR requirements. Ceramic capacitors are manufactured with a variety of dielectrics, each with a different behavior over temperature and applied voltage. Capacitors must have an adequate dielectric to ensure the minimum capacitance over the necessary temperature range and dc bias conditions. X5R or X7R dielectrics with a voltage rating of 6.3 V or 10 V are recommended. Y5V and Z5U dielectrics are not recommended, due to their poor temperature and dc bias characteristics.

Figure 49 depicts the capacitance vs. voltage bias characteristic of an 0402 1  $\mu\text{F}$ , 10 V, X5R capacitor. The voltage stability of a capacitor is strongly influenced by the capacitor size and voltage rating. In general, a capacitor in a larger package or higher voltage rating exhibits better stability. The temperature variation of the X5R dielectric is about  $\pm 15\%$  over the  $-40^\circ\text{C}$  to  $+85^\circ\text{C}$  temperature range and is not a function of the package or voltage rating.

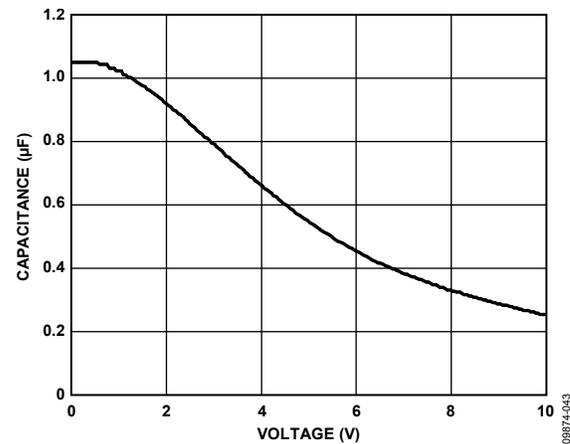


Figure 49. Capacitance vs. Voltage Bias Characteristic

Use Equation 1 to determine the worst-case capacitance accounting for capacitor variation over temperature, component tolerance, and voltage.

$$C_{EFF} = C_{BIAS} \times (1 - TEMPCO) \times (1 - TOL) \quad (1)$$

where:

$C_{BIAS}$  is the effective capacitance at the operating voltage.  
 $TEMPCO$  is the worst-case capacitor temperature coefficient.  
 $TOL$  is the worst-case component tolerance.

In this example,  $TEMPCO$  over  $-40^{\circ}\text{C}$  to  $+85^{\circ}\text{C}$  is assumed to be 15% for an X5R dielectric.  $TOL$  is assumed to be 10%, and  $C_{BIAS}$  is  $0.94\ \mu\text{F}$  at 1.8 V from the graph in Figure 49.

Substituting these values into Equation 1 yields

$$C_{EFF} = 0.94\ \mu\text{F} \times (1 - 0.15) \times (1 - 0.1) = 0.719\ \mu\text{F}$$

Therefore, the capacitor chosen in this example meets the minimum capacitance requirement of the LDO over temperature and tolerance at the chosen output voltage.

To guarantee the performance of the ADP320 triple LDO, it is imperative that the effects of dc bias, temperature, and tolerances on the behavior of the capacitors are evaluated for each application.

### UNDERVOLTAGE LOCKOUT

The ADP320 triple LDO has an internal undervoltage lockout circuit that disables all inputs and the output when the input voltage bias,  $V_{BIAS}$ , is less than approximately 2.2 V. This ensures that the inputs of the ADP320 triple LDO and the output behave in a predictable manner during power-up.

### ENABLE FEATURE

The ADP320 triple LDO uses the ENx pins to enable and disable the  $V_{OUTx}$  pins under normal operating conditions. Figure 50 shows a rising voltage on EN crossing the active threshold, then  $V_{OUTx}$  turns on. When a falling voltage on ENx crosses the inactive threshold,  $V_{OUTx}$  turns off.

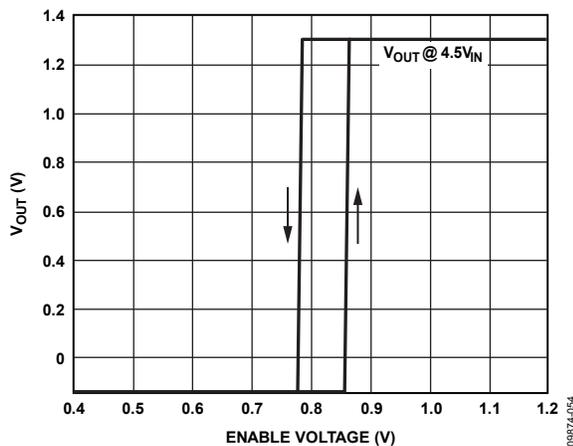


Figure 50. Typical ENx Pin Operation

As shown in Figure 50, the ENx pin has built-in hysteresis. This prevents on/off oscillations that can occur due to noise on the ENx pin as it passes through the threshold points.

The active/inactive thresholds of the ENx pin are derived from the  $V_{BIAS}$  voltage. Therefore, these thresholds vary with changing input voltage. Figure 51 shows typical ENx active/inactive thresholds when the input voltage varies from 2.5 V to 5.5 V.

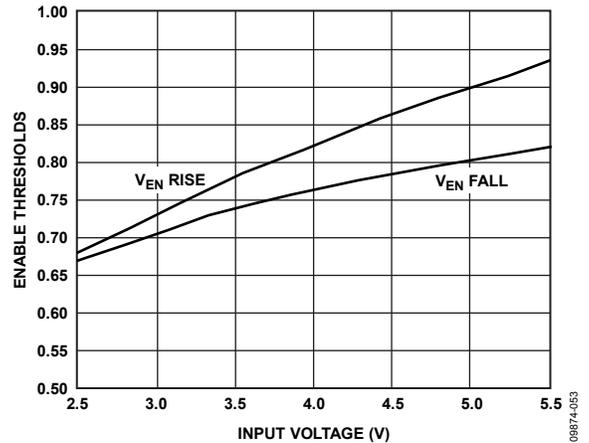


Figure 51. Typical ENx Pins Thresholds vs. Input Voltage

The ADP320 triple LDO utilizes an internal soft start to limit the inrush current when the output is enabled. The start-up time for the 2.8 V option is approximately 220  $\mu\text{s}$  from the time the ENx active threshold is crossed to when the output reaches 90% of its final value. The start-up time is somewhat dependent on the output voltage setting and increases slightly as the output voltage increases.

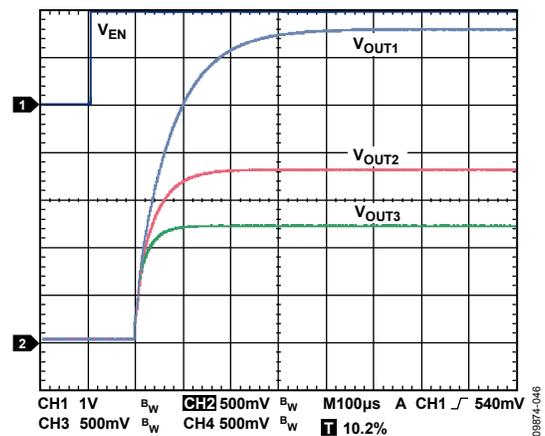


Figure 52. Typical Start-Up Time,  
 $I_{LOAD1} = I_{LOAD2} = I_{LOAD3} = 100\ \text{mA}$ ,  
 $CH1 = V_{EN}$ ,  $CH2 = V_{OUT1}$ ,  $CH3 = V_{OUT2}$ ,  $CH4 = V_{OUT3}$

## CURRENT-LIMIT AND THERMAL OVERLOAD PROTECTION

The ADP320 triple LDO is protected against damage due to excessive power dissipation by current and thermal overload protection circuits. The ADP320 triple LDO is designed to current limit when the output load reaches 300 mA (typical). When the output load exceeds 300 mA, the output voltage is reduced to maintain a constant current limit.

Thermal overload protection is built-in, which limits the junction temperature to a maximum of 155°C (typical). Under extreme conditions (that is, high ambient temperature and power dissipation) when the junction temperature starts to rise above 155°C, the output is turned off, reducing the output current to zero. When the junction temperature drops below 140°C, the output is turned on again and the output current is restored to its nominal value.

Consider the case where a hard short from VOUTx to GND occurs. At first, the ADP320 triple LDO current limits, so that only 300 mA is conducted into the short. If self-heating of the junction is great enough to cause its temperature to rise above 155°C, thermal shutdown activates turning off the output and reducing the output current to zero. As the junction temperature cools and drops below 140°C, the output turns on and conducts 300 mA into the short, again causing the junction temperature to rise above 155°C. This thermal oscillation between 140°C and 154°C causes a current oscillation between 0 mA and 300 mA that continues as long as the short remains at the output.

Current and thermal limit protections are intended to protect the device against accidental overload conditions. For reliable operation, device power dissipation must be externally limited so junction temperatures do not exceed 125°C.

## THERMAL CONSIDERATIONS

In most applications, the ADP320 triple LDO does not dissipate a lot of heat due to high efficiency. However, in applications with a high ambient temperature and high supply voltage to output voltage differential, the heat dissipated in the package is large enough that it can cause the junction temperature of the die to exceed the maximum junction temperature of 125°C.

When the junction temperature exceeds 155°C, the converter enters thermal shutdown. It recovers only after the junction temperature has decreased below 140°C to prevent any permanent damage. Therefore, thermal analysis for the chosen application is very important to guarantee reliable performance over all conditions. The junction temperature of the die is the sum of the ambient temperature of the environment and the temperature rise of the package due to the power dissipation, as shown in Equation 2.

To guarantee reliable operation, the junction temperature of the ADP320 triple LDO must not exceed 125°C. To ensure that the junction temperature stays below this maximum value, the user needs to be aware of the parameters that contribute to junction temperature changes. These parameters include ambient temperature, power dissipation in the power device, and thermal resistances between the junction and ambient air ( $\theta_{JA}$ ). The  $\theta_{JA}$  number is dependent on the package assembly compounds used and the amount of copper to which the GND pins of the package are soldered on the PCB. Table 6 shows typical  $\theta_{JA}$  values for the ADP320 triple LDO for various PCB copper sizes.

**Table 6. Typical  $\theta_{JA}$  Values**

Copper Size (mm <sup>2</sup> )	ADP320 Triple LDO (°C/W)
JEDEC <sup>1</sup>	49.5
100	83.7
500	68.5
1000	64.7

<sup>1</sup> Device soldered to JEDEC standard board.

The junction temperature of the ADP320 triple LDO can be calculated from the following equation:

$$T_J = T_A + (P_D \times \theta_{JA}) \quad (2)$$

where:

$T_A$  is the ambient temperature.

$P_D$  is the power dissipation in the die, given by

$$P_D = \Sigma[(V_{IN} - V_{OUT}) \times I_{LOAD}] + \Sigma(V_{IN} \times I_{GND}) \quad (3)$$

where:

$I_{LOAD}$  is the load current.

$I_{GND}$  is the ground current.

$V_{IN}$  and  $V_{OUT}$  are input and output voltages, respectively.

Power dissipation due to ground current is quite small and can be ignored. Therefore, the junction temperature equation simplifies to

$$T_J = T_A + \{\Sigma[(V_{IN} - V_{OUT}) \times I_{LOAD}] \times \theta_{JA}\} \quad (4)$$

As shown in Equation 4, for a given ambient temperature, input-to-output voltage differential, and continuous load current, there exists a minimum copper size requirement for the PCB to ensure the junction temperature does not rise above 125°C. Figure 53 to Figure 56 show junction temperature calculations for different ambient temperatures, total power dissipation, and areas of PCB copper.

In cases where the board temperature is known, the thermal characterization parameter,  $\Psi_{JB}$ , may be used to estimate the junction temperature rise.  $T_J$  is calculated from  $T_B$  and  $P_D$  using the formula

$$T_J = T_B + (P_D \times \Psi_{JB}) \quad (5)$$

The typical  $\Psi_{JB}$  value for the 16-lead 3 mm × 3 mm LFCSP is 25.2°C/W.

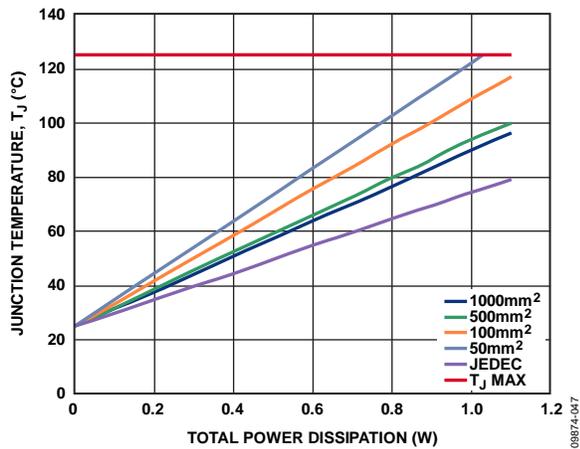


Figure 53. Junction Temperature vs. Total Power Dissipation,  $T_A = 25^\circ\text{C}$

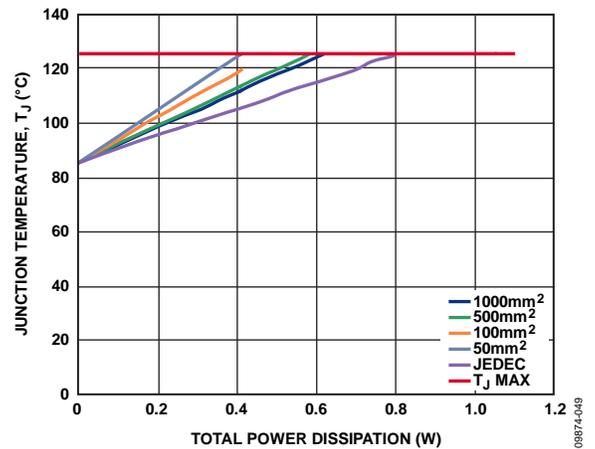


Figure 55. Junction Temperature vs. Total Power Dissipation,  $T_A = 85^\circ\text{C}$

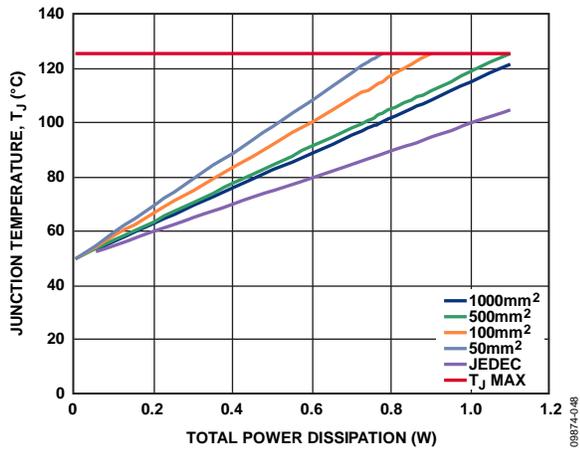


Figure 54. Junction Temperature vs. Total Power Dissipation,  $T_A = 50^\circ\text{C}$

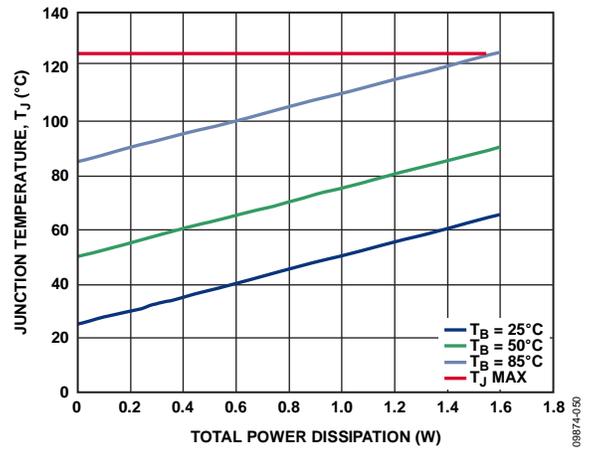


Figure 56. Junction Temperature vs. Total Power Dissipation and Board Temperature

**PRINTED CIRCUIT BOARD LAYOUT CONSIDERATIONS**

Heat dissipation from the package can be improved by increasing the amount of copper attached to the pins of the ADP320 triple LDO. However, as can be seen from Table 6, a point of diminishing returns eventually is reached, beyond which an increase in the copper size does not yield significant heat dissipation benefits.

Place the input capacitor as close as possible to the VINx and GND pins. Place the output capacitors as close as possible to the VOUTx and GND pins. Use 0402 or 0603 size capacitors and resistors to achieve the smallest possible footprint solution on boards where area is limited.

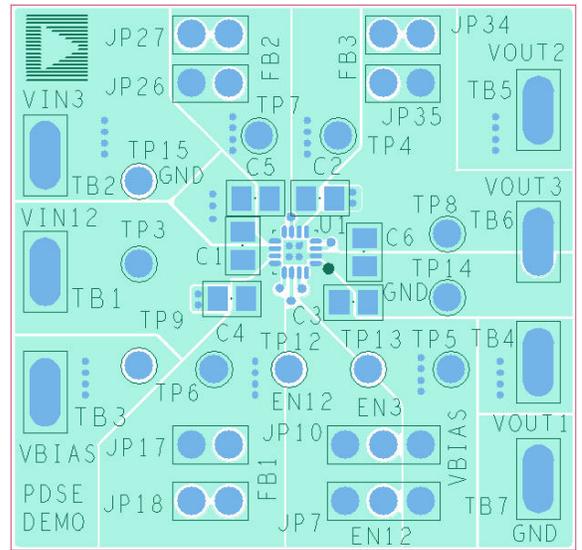


Figure 57. Example of PCB Layout, Top Side

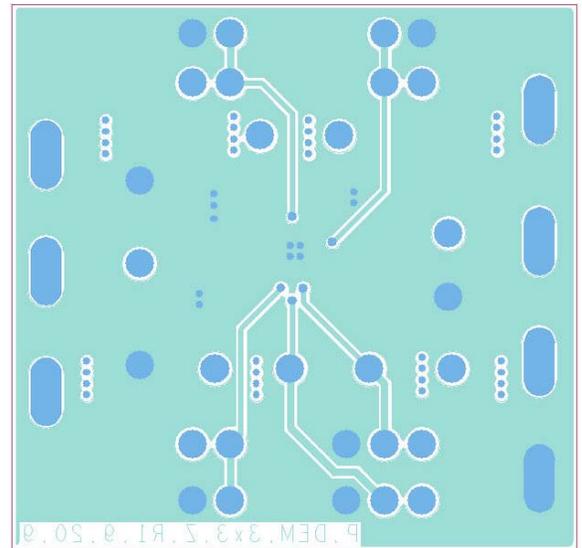
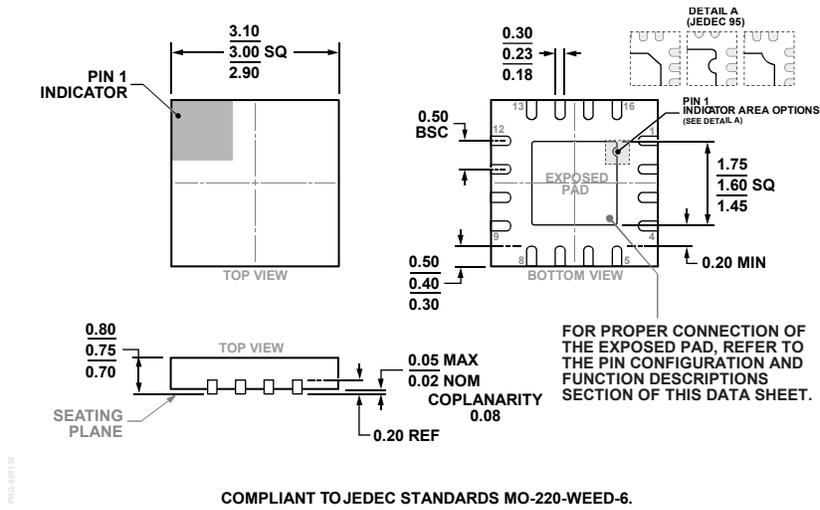


Figure 58. Example of PCB Layout, Bottom Side

# OUTLINE DIMENSIONS



COMPLIANT TO JEDEC STANDARDS MO-220-WEED-6.

Figure 59. 16-Lead Lead Frame Chip Scale Package [LFCSP]  
 3 mm × 3 mm Body and 0.75 mm Package Height  
 (CP-16-22)  
 Dimensions shown in millimeters

## ORDERING GUIDE

Model <sup>1</sup>	Temperature Range	Output Voltage (V) <sup>2</sup>	Package Description	Package Option	Branding
ADP320ACPZ331815R7	-40°C to +125°C	3.3, 1.8, 1.5	16-Lead LFCSP	CP-16-22	LGP
ADP320ACPZ-110-R7	-40°C to +125°C	3.3, 3.3, 1.5	16-Lead LFCSP	CP-16-22	L15

<sup>1</sup> Z = RoHS Compliant Part.

<sup>2</sup> For additional voltage options, contact a local Analog Devices sales or distribution representative.